

January 26, 2021

Mr. David R. Consigli
Chairman
Town of Milford - Zoning Board of Appeals (ZBA)
52 Main Street
Milford, MA

Re: The Residences at Stone Ridge - Phase II

Response to Sewer Department Comments

SMMA No. 19162

Dear Mr. Consigli:

On behalf of our client, The Gutierrez Company (TGC), SMMA has prepared the response below to the Sewer Review letters prepared by Tata & Howard (T&H), dated September 28, 2020 and November 17, 2020. Attached with this letter are the requested pump system details including pump station calculations, pump technical data, and two exhibits showing the proposed 19,000-gallon emergency storage tank.

Per the suggestions in Tata & Howard's September 28, 2020 Sewer Review letter, we propose to eliminate the Upper Deer Street Pump Station and instead provide additional emergency storage at the Lower Deer Street Pump Station. The 8 ft and 10 ft diameter pump stations will remain (bottom of tanks = 284.13, pump range = 286.0 – 287.5). We propose a 19,000 gallon emergency storage tank beneath Deer Street connected to the original 8 ft diameter pump station with two equalization pipes. The equalization pipes and the proposed emergency storage tank bottom will be at upper pump range elevation = 287.5. The emergency storage tank will be located 10 ft from the water main and hydrant service. It will require realigning a short segment of the existing 6" force main around the proposed emergency tank. In the event the tank requires maintenance or cleaning, the tank will have two 24" diameter manhole access covers and there will be direct access from Deer Street. This storage tank will provide sufficient capacity for all of the remaining developable land.

We look forward to discussing this information with the Town of Milford Board of Sewer Commissioners and their consultant, Tata & Howard. If you have any questions, please feel free to contact me at 617-520-9210 or wpark@smma.com.

Very truly yours,

SMMA



William Park, PE
Senior Associate | Civil Engineer

cc: Israel Lopez - The Gutierrez Company, Peter Glick - SMMA, (MF)

enclosures: Pump Station Design Calculations and Exhibits

1000 MASSACHUSETTS AVENUE
CAMBRIDGE, MASSACHUSETTS 02138
T: 617.547.5400

Stone Ridge
SMMA #19162

Date: 12/04/2020, Rev. 01/25/2021

Pump Station Design - Currently Proposed -w/Modified & New Pump Station Configuration

I. PUMP STATION DESIGN INFORMATION

Use	Quantity	Unit	Rate		GPD	Hours Op.	Adj. Max. Flow (GPM)	Peak Factor	Peak Flow (GPD)	Adj. Peak Flow (GPM)
Restaurant Depot	63,085	sq. ft.	50	per 1000 sq. ft.	3,154	12	4.38	3.0	9,463	13
Residences - Phase I	383	bedrooms	110	per bedroom	42,130	18	39.01	4.0	168,520	156
Residences - Phase II	460	bedrooms	110	per bedroom	50,600	18	46.85	4.0	202,400	187
Swimming Pool	104	persons	10	gpd/person	1,040	18	0.96	4.0	4,160	4
I/I	1,450	li. ft.	200	gpd/idm	439	24	0.30	4.0	1,756	1
Future Development	Conceptual Design Flow				21,120	12	29.33	3.0	63,360	88
Total					118,483		121		449,659	450

B. High Point in Force Main (ft) = 304.00
Pump Off Elevation (ft) = 286.00
Elevation Head (ft) = 18.00

C. Force Main Velocity Check: Dia.(in) = 6
Length (ft) = 2347
Assumed Q_{pump} (gpm) = 475
Material = PVC
* Velocity (ft/s) = 5.39
Hazen-Williams "C" value = 140

* (3.00 ft/s < velocity < 7.00 ft/s)

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D. Minor Losses in Fittings "K" Value (Included in Total Equivalent Length)

Apparatus	Quantity	"K" Value	Quantity * K
Check Valve	1	1.80	1.80
Enlargement	0	0.10	0.00
90° Bend	4	0.54	2.16
6" Gate Valve	1	0.14	0.14
Tee Branch	0	1.08	0
Tee Through	0	0.36	0.00
45° Bend	8	0.29	2.32
22.5° Bend	0	0.24	0.00
Pipe Exit	1	1.00	1.00
Total "K" =			7.42

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II. SYSTEM HEAD COMUTATIONS

Given: Forcemain Diameter (in) = 6
 Length of Forcemain (ft) = 2347
 Hazen-Williams "C" Value = 140
 Minor Loss "K" Value = 7.42
 High Point Elevation (ft) = 304.00
 Pump Off Elevation (ft) = 286.00

Minor Headloss (Hm) = $K \cdot (V^2) / (2 \cdot G)$

Friction Headloss (Hf) = $2.083 \cdot (L/1000)^{1.85} \cdot (\text{gpm}^{1.85} / \text{dia}^{4.8655})$

Static Headloss (Hstat) = Discharge Elevation - Pump Off Elevation

Total Dynamic Head (TDH) = Hm + Hf + Hstat

Q (gmp)	V (fps)	Hm (ft)	Hf (ft)	Hstat (ft)	TDH	
0	0.00	0.00	0.00	18.00	18.00	
25	0.28	0.01	0.17	18.00	18.17	
50	0.57	0.04	0.60	18.00	18.63	
75	0.85	0.08	1.26	18.00	19.35	
100	1.14	0.15	2.15	18.00	20.30	
125	1.42	0.23	3.25	18.00	21.48	
150	1.70	0.33	4.56	18.00	22.89	
175	1.99	0.45	6.06	18.00	24.51	
200	2.27	0.59	7.76	18.00	26.35	
225	2.55	0.75	9.65	18.00	28.40	
250	2.84	0.93	11.72	18.00	30.65	
275	3.12	1.12	13.98	18.00	33.10	
300	3.41	1.34	16.42	18.00	35.76	
325	3.69	1.57	19.04	18.00	38.61	
350	3.97	1.82	21.84	18.00	41.66	
375	4.26	2.09	24.82	18.00	44.90	
400	4.54	2.38	27.96	18.00	48.34	
425	4.83	2.68	31.28	18.00	51.96	
450	5.11	3.01	34.77	18.00	55.78	
475	5.39	3.35	38.43	18.00	59.78	Qpump
500	5.68	3.71	42.25	18.00	63.97	
525	5.96	4.09	46.25	18.00	68.34	
550	6.24	4.49	50.40	18.00	72.89	
575	6.53	4.91	54.72	18.00	77.63	
600	6.81	5.35	59.20	18.00	82.55	

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III. WETWELL DESIGN

A. Volume of Wetwell

$$V = t * q / 4$$

t = minimum cycle time (min)
q = peak flow (gpm)
V = volume (gal)

t = 15
q = 29

V = 109

B. Wetwell & Pump Elevations:

298.00	Top of Slab
290.00	Invert In
288.00	Lag Pump On & High Water Alarm
287.50	Lead Pump On
286.00	Pumps Off and Alternate
285.80	Low Water Alarm
284.80	Bottom Inside of Chamber

C. Effective Capacity of Wetwell Chamber:

	Wetwell A	Wetwell B
Inside Dia. (ft) =	8.00	10.00
X - Area (sf) =	50.3	78.5
Effective Capacity (gal) =	564	881

Total Capacity Wetwell A + Wetwell B = 1,445

D. Emergency Storage Capacity:

Wetwells A & B Above "Pump On" Elevation to Underside of Slab =	9,471	Gal.
Emergency Storage Tank (ID = 36'-5" L x 10'-0" W x 8'-0" H) Above "HWA" Elevation (288.0) to Underside of Tank Slab (296.0) =	20,645	Gal.
Total =	30,116	Gal.

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IV. WETWELL DETENTION TIMES

A. Time to Empty Wetwell (pump run start to stop)

$$T1 = \text{Effective Capacity} / (Q_{\text{pump}} - Q_{\text{in}})$$

Effective Capacity (gal) =	1445
Pumping Rate (gpm) =	475
Max. Daily Flow (gpd) =	118,483
Peak Flow (gpm) =	450
Max. Daily Flow (gpm) =	121

1. No Inflow:	T1(min) =	3.04
2. Maximum Daily Inflow:	T1(min) =	4.08
3. Peak Inflow:	T1(min) =	57.03
4. 1/2 Of Pump Rate:	T1(min) =	6.09

B. Time to Fill Wetwell (pump off)

$$T2 = \text{Effective Capacity} - Q_{\text{in}}$$

1. No Inflow:	T2(min) =	N/A
2. Maximum Daily Inflow:	T2(min) =	11.96
3. Peak Inflow:	T2(min) =	3.21
4. 1/2 Of Pump Rate:	T2(min) =	6.09

C. Cycle Time (pump start to start)

$$Tt = T1 + T2$$

1. No Inflow:	Tt(min) =	N/A
2. Maximum Daily Inflow:	Tt(min) =	16.04
3. Peak Inflow:	Tt(min) =	60.24
4. 1/2 Of Pump Rate:	Tt(min) =	12.17

NP 3153 HT 3~ 465

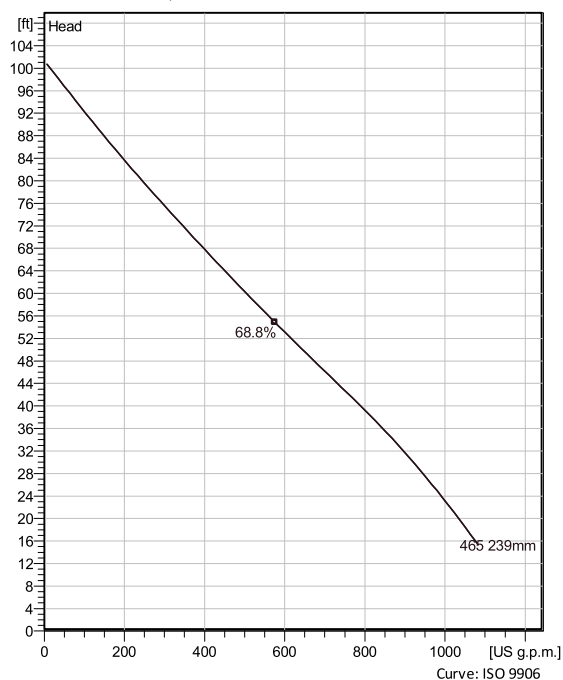
Patented self cleaning semi-open channel impeller, ideal for pumping in waste water applications. Possible to be upgraded with Guide-pin® for even better clogging resistance. Modular based design with high adaptation grade.



Technical specification



Curves according to: Water, pure ,39.2 °F,62.42 lb/ft³,1.6891E-5 ft²/s



Configuration

Motor number N3153.830 21-15-4AS-W IE3 14hp	Installation type P - Semi permanent, Wet
Impeller diameter 239 mm	Discharge diameter 4 inch

Pump information

Impeller diameter 239 mm
Discharge diameter 4 inch
Inlet diameter 150 mm
Maximum operating speed 1800 rpm
Number of blades 2
Max. fluid temperature 40 °C

Materials

Impeller Hard-Iron™

Project	Created by	Ian Belczyk	Last update	12/8/2020
Block	Created on	12/8/2020		

NP 3153 HT 3~ 465

Technical specification



Motor - General

Motor number N3153.830 21-15-4AS-W IE3 14hp	Phases 3~	Rated speed 1800 rpm	Rated power 14 hp
ATEX approved FM	Number of poles 4	Rated current 14 A	Stator variant 15
Frequency 60 Hz	Rated voltage 460 V	Insulation class H	Type of Duty S1
Version code 830			

Motor - Technical

Power factor - 1/1 Load 0.98	Motor efficiency - 1/1 Load 92.8 %	Total moment of inertia 1.96 lb ft ²	Starts per hour max. 30
Power factor - 3/4 Load 0.97	Motor efficiency - 3/4 Load 92.7 %	Starting current, direct starting 129 A	
Power factor - 1/2 Load 0.96	Motor efficiency - 1/2 Load 91.2 %	Starting current, star-delta 43 A	

Project
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NP 3153 HT 3~ 465

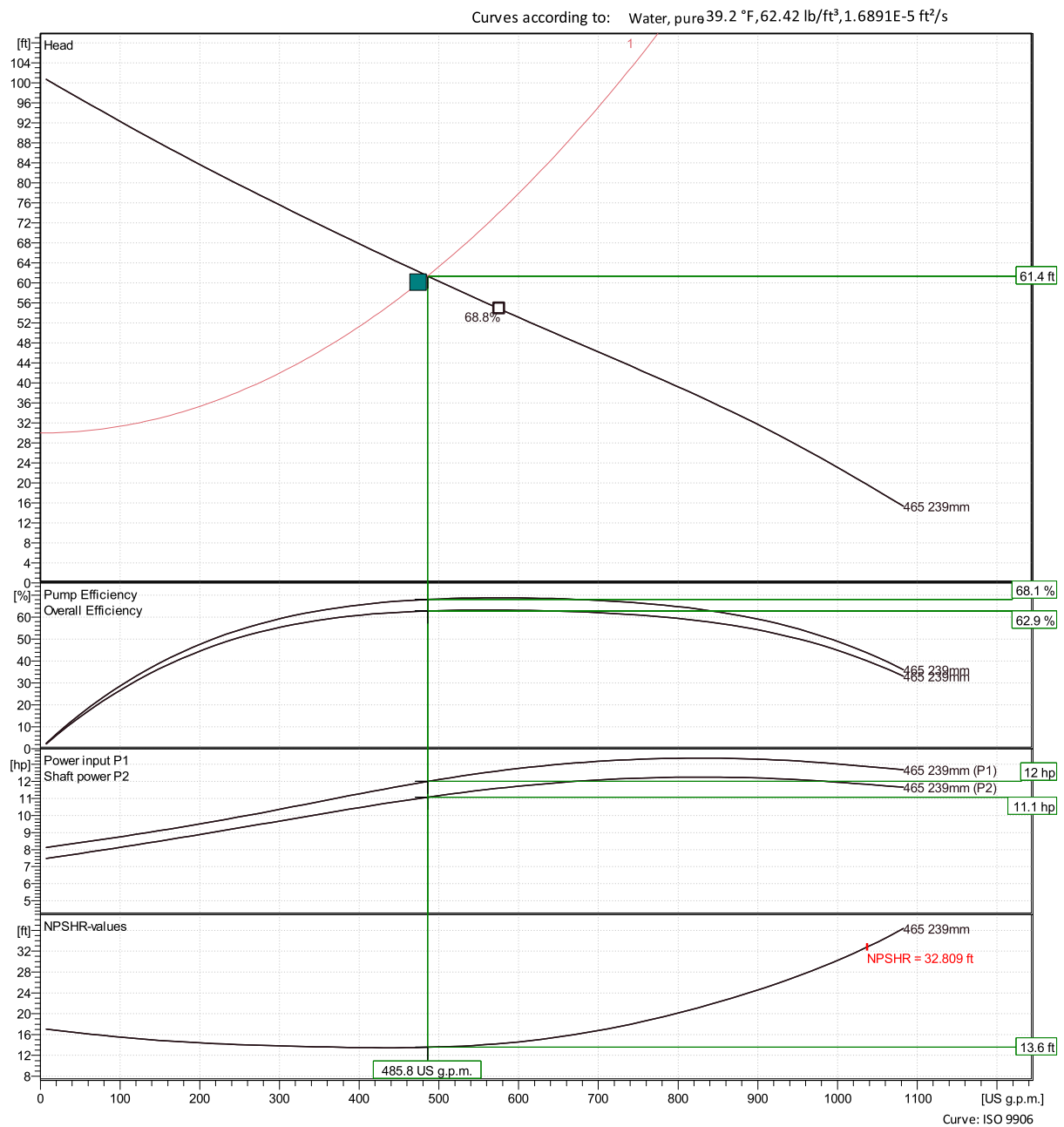
Performance curve



Duty point

Flow
486 US g.p.m.

Head
61.4 ft



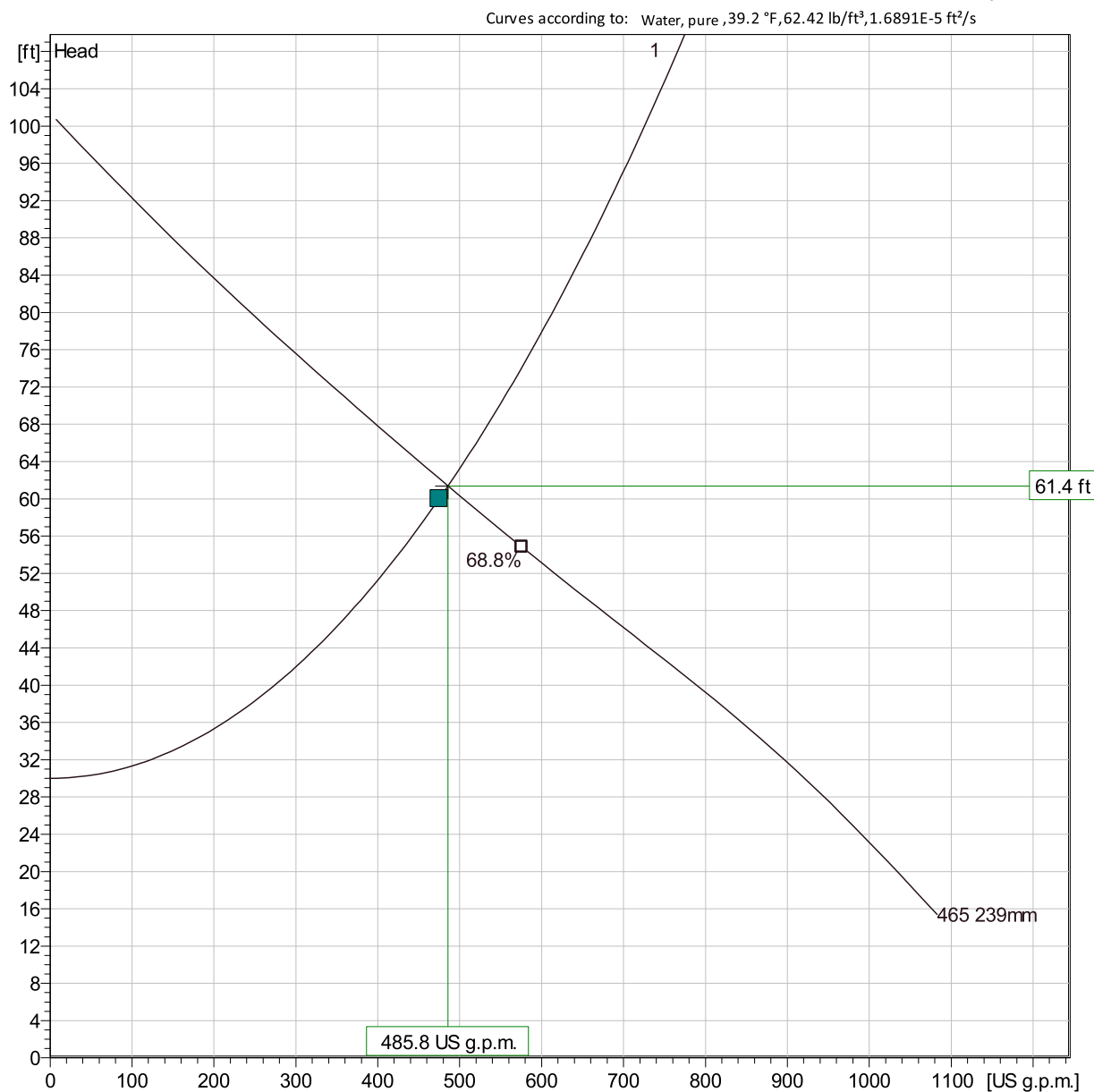
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NP 3153 HT 3~ 465

Duty Analysis



Operating characteristics

Pumps / Systems	Flow	Head	Shaft power	Flow	Head	Shaft power	Hydr.eff.	Specific Energy	NPSHre
1	486 US g.p.m.	61.4 ft	11.1 hp	486 US g.p.m.	61.4 ft	11.1 hp	68.1 %	307 kWh/US M	13.6 ft

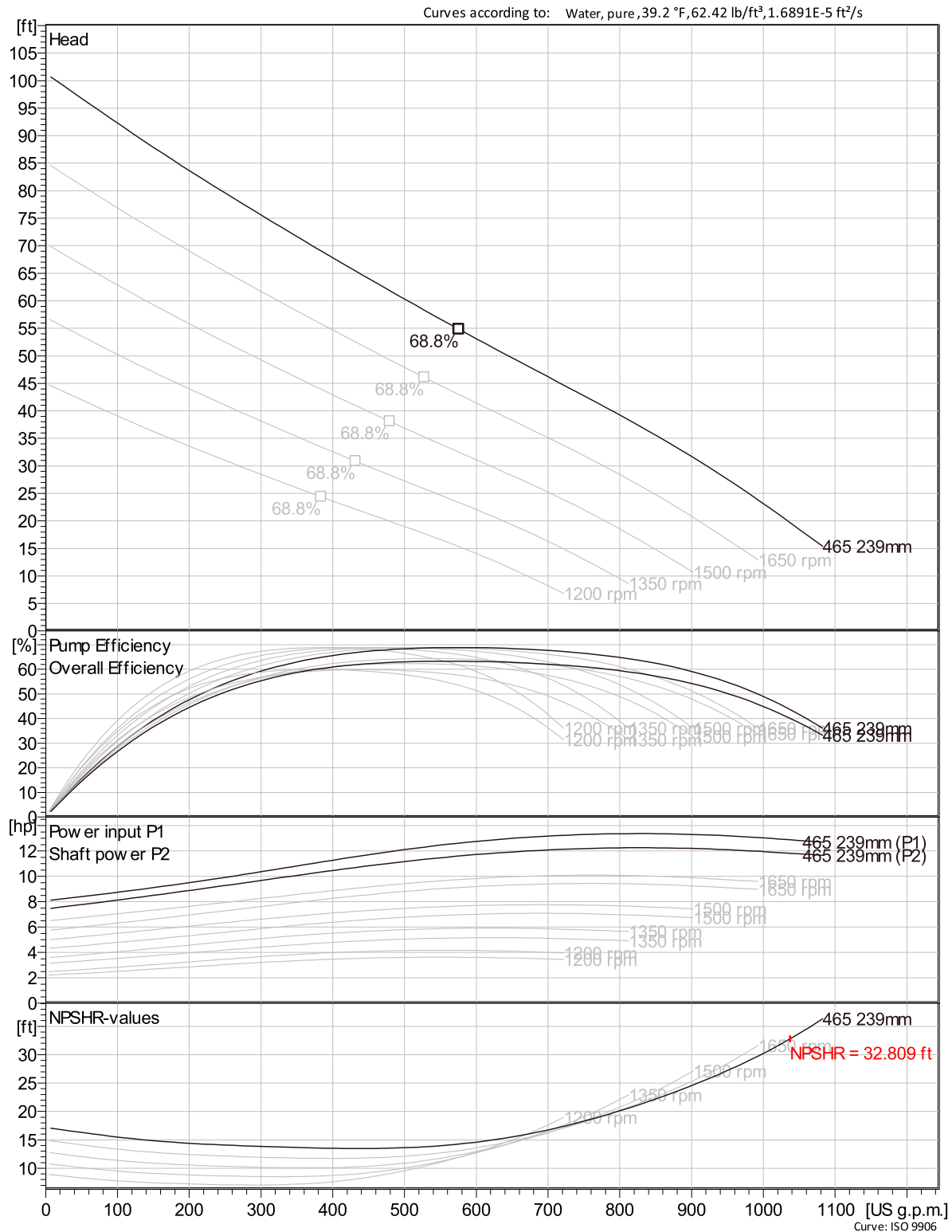
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VFD Curve



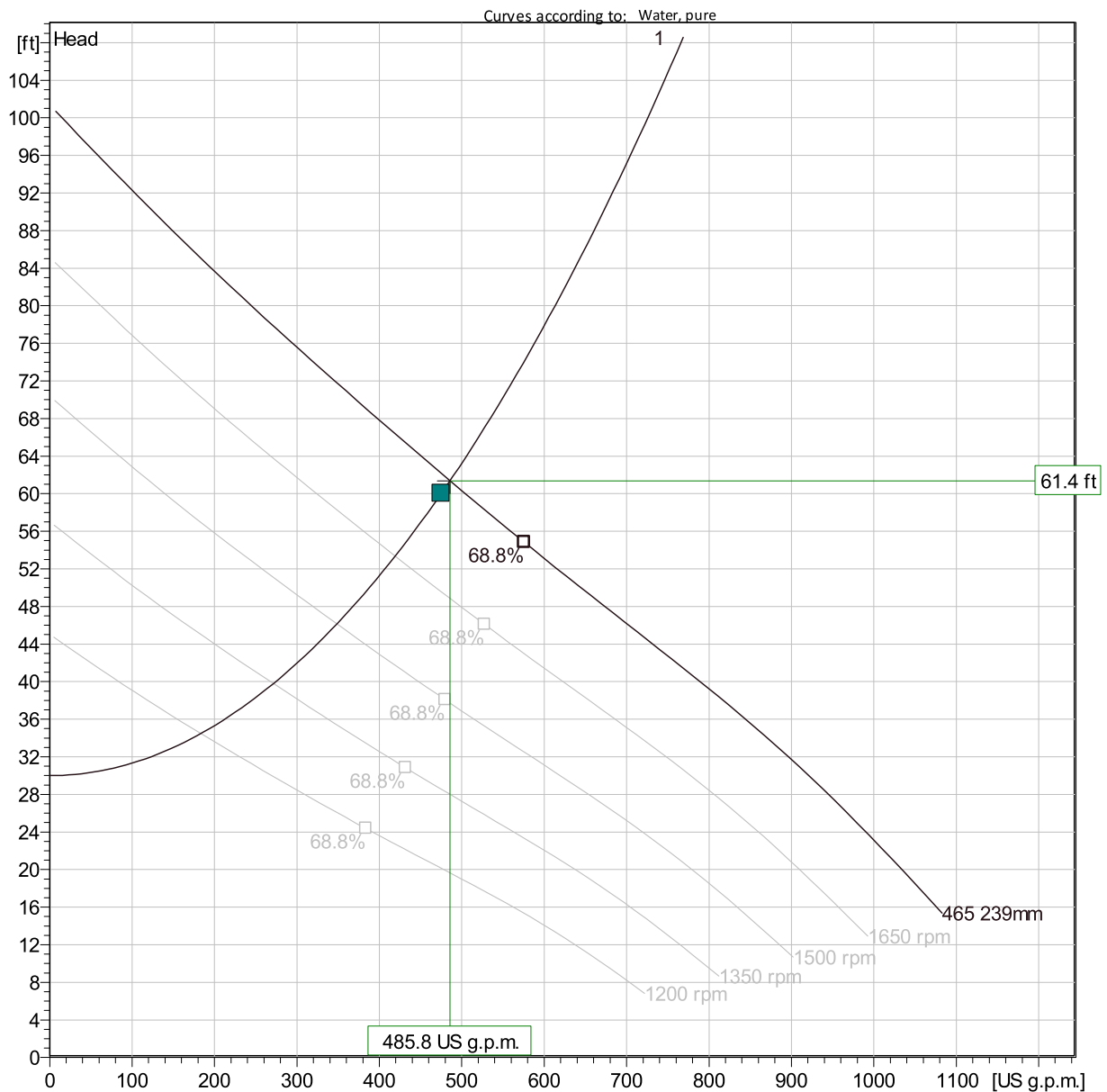
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NP 3153 HT 3~ 465

VFD Analysis



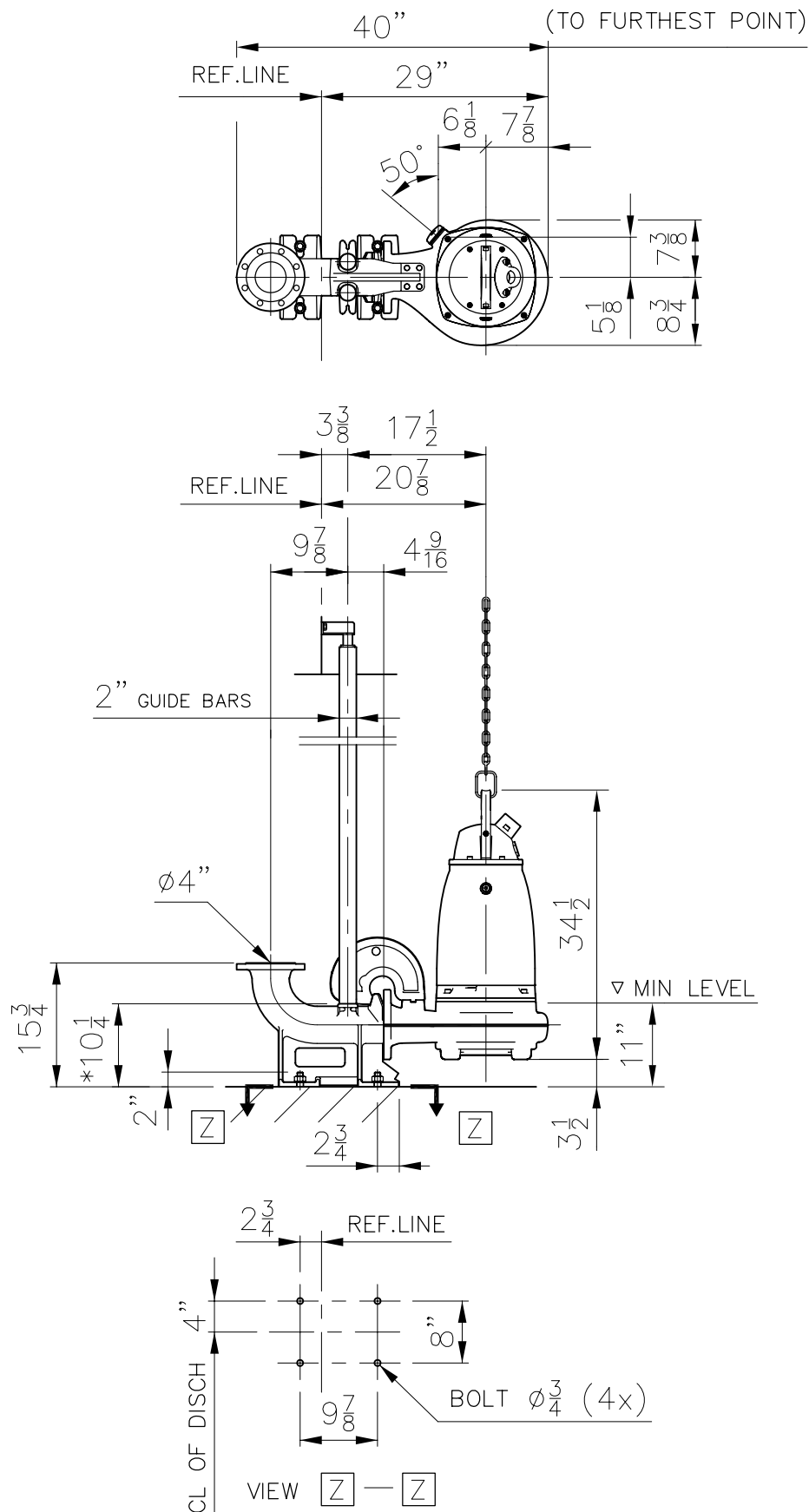
Operating characteristics

Pumps / Systems	Frequency	Flow	Head	Shaft power	Flow	Head	Shaft power	Hydr.eff.	Specific Energy	NPSHre
1	60 Hz	486 US g.p.m.	61.4 ft	11.1 hp	486 US g.p.m.	61.4 ft	11.1 hp	68.1 %	307 kWh/US M	13.6 ft
1	55 Hz	419 US g.p.m.	53.4 ft	8.38 hp	419 US g.p.m.	53.4 ft	8.38 hp	67.5 %	267 kWh/US M	11.7 ft
1	50 Hz	348 US g.p.m.	46.1 ft	6.13 hp	348 US g.p.m.	46.1 ft	6.13 hp	66.3 %	245 kWh/US M	10.1 ft
1	45 Hz	271 US g.p.m.	39.8 ft	4.29 hp	271 US g.p.m.	39.8 ft	4.29 hp	63.7 %	227 kWh/US M	8.59 ft
1	40 Hz	183 US g.p.m.	34.5 ft	2.81 hp	183 US g.p.m.	34.5 ft	2.81 hp	57 %	216 kWh/US M	7.29 ft

Project
Block

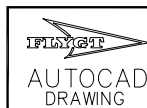
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Created on 12/8/2020

Last update 12/8/2020



* DIMENSION TO ENDS OF GUIDE BARS

Weight (lbs)	
Pump	Disch
465	95



Denomination
Dimensional drwg
NP,FP 3153 HT
ø4"

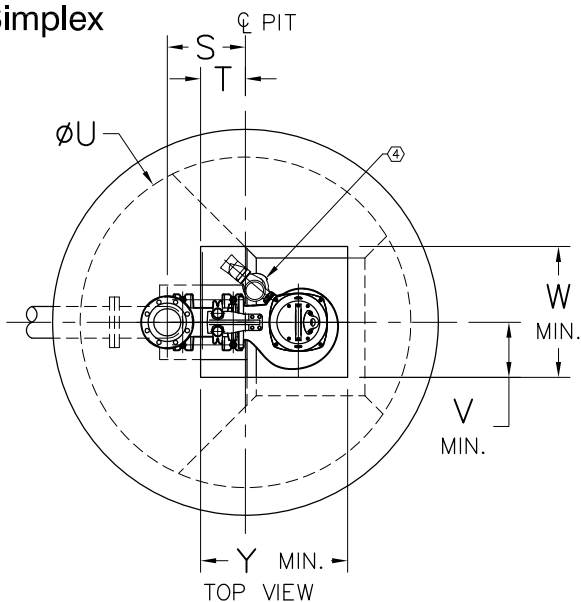
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Scale		Reg no 5399
6504500		11

FP/NP-3153

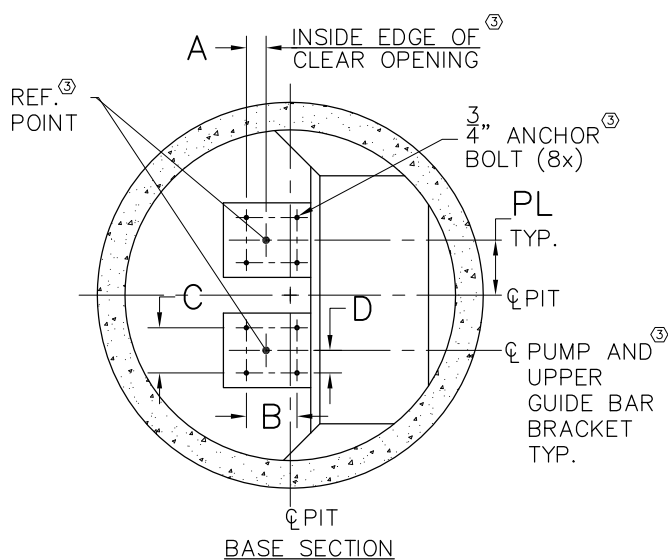
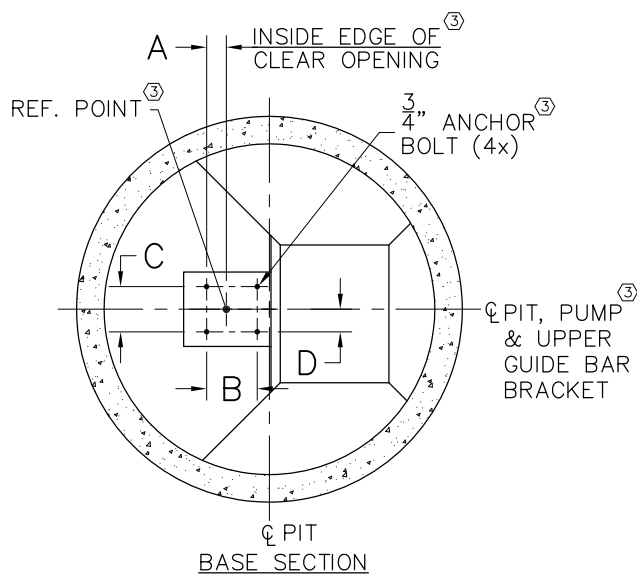
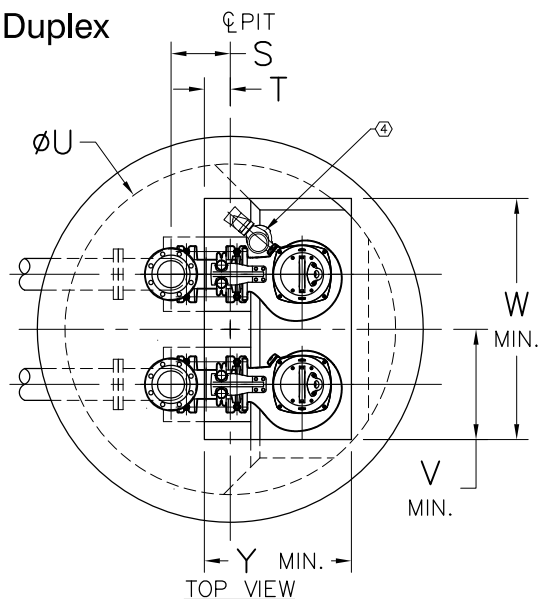
NOTES:

1. CONFIGURATION AND DIMS. SHOWN ARE SUGGESTED REQUIREMENTS ONLY. ALL DETAILS, INCLUDING SIZING OF PIT, TYPE, LOCATION AND ARRANGEMENT OF VALVES AND PIPING, ETC. ARE TO BE SPECIFIED BY THE CONSULTING ENGINEER AND ARE SUBJECT TO THEIR APPROVAL.
2. REFERENCE GENERIC DUPLEX LIFT STATION LAYOUT FOR ELEVATION VIEW.
3. LOCATE ANCHOR BOLTS USING INSIDE EDGE OF CLEAR OPENING AND PUMP CENTERLINE AS REFERENCE POINT. BOLT LOCATIONS MUST BE HELD TO MAINTAIN EXACT POSITION OF PUMP TO CLEAR OPENING.
4. ITT FLYGT MIX-FLUSH VALVE.

Simplex

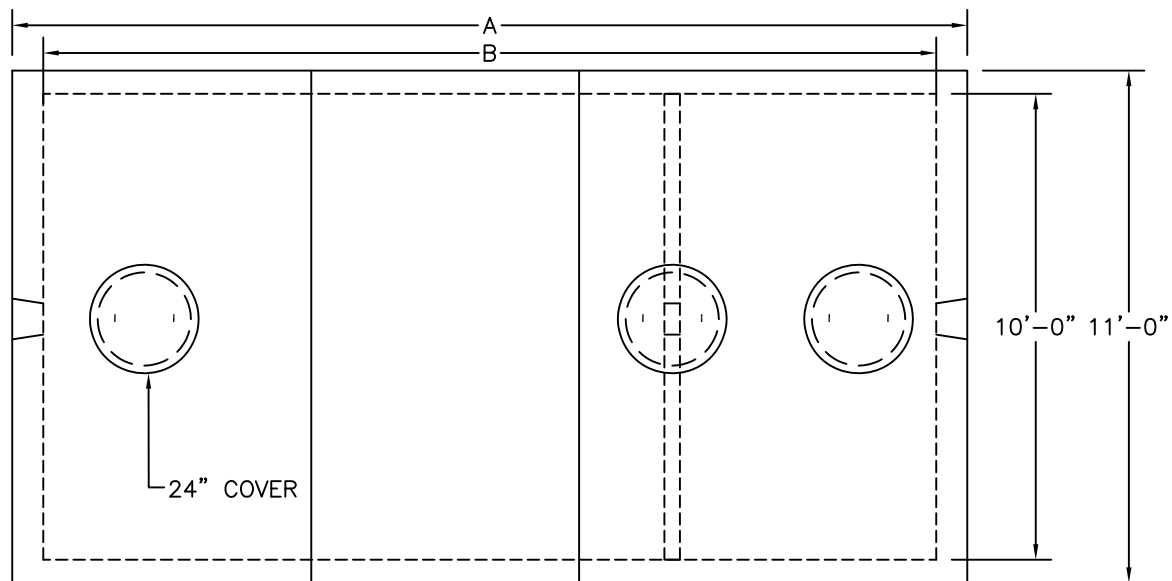


Duplex

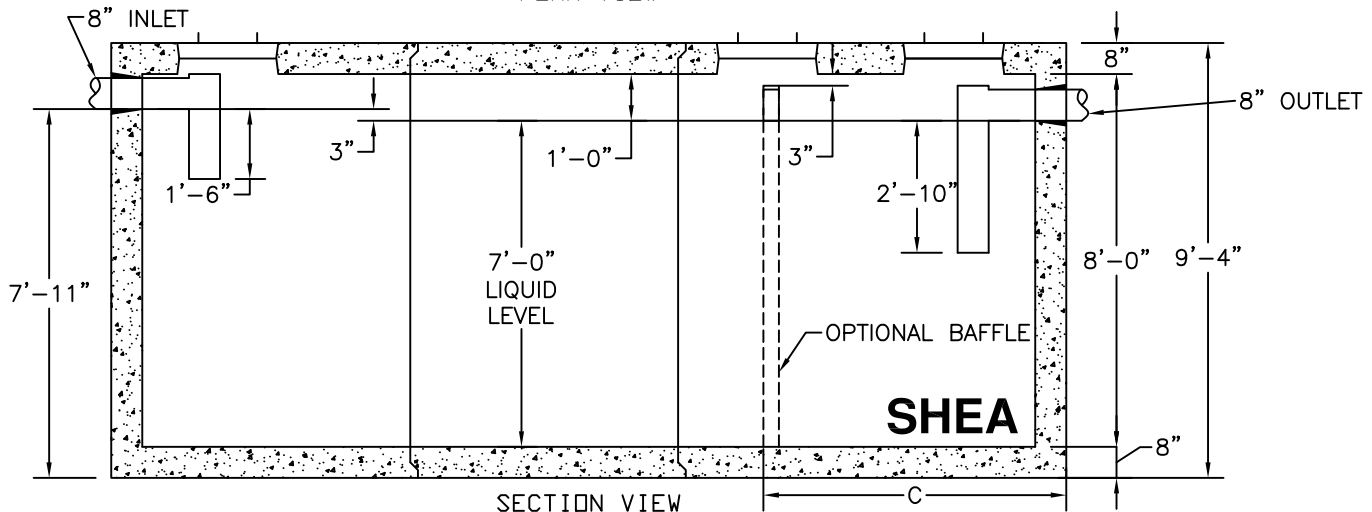


ALL DIMENSIONS ARE IN INCHES

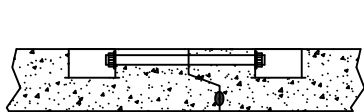
MODEL	NOM. SIZE	VERSION	SIMPLEX										DUPLEX						
			A	B	C	D	S	T	U	V	W	Y	S	T	U	PL	V	W	Y
FP/NP	3"	SH	2 1/2	9 7/8	8	4	21 1/4	15 1/4	72	9	27	29 1/2	18 3/8	12 3/8	72	11	20	49	29 1/2
FP/NP	4"	SH	2 3/4	9 7/8	8	4	19 3/4	13 1/4	72	9	27	29 1/2	16 1/2	10	72	11	20	49	29 1/2
FP/NP	4"	HT	2 3/4	9 7/8	8	4	19 3/4	13 1/4	72	11	27 1/2	30 1/2	16 1/2	10	72	11	22	49 1/2	30 1/2
FP/NP	6"	MT	4 5/8	11	10	5	17 5/8	9 3/4	72	12	28 1/2	32	12 5/8	5 1/4	72	12	24	52 1/2	32
NP	8"	LT	5 1/2	11	10	5	14 1/4	5 3/8	72	14	30 1/2	35	16 1/2	7 3/8	84	13	27	56 1/2	35
NP	10"	LT	14 3/8	19 3/4	10	5	23 3/4	13	96	16 1/2	35 1/2	40	16 3/4	6	96	18	34 1/2	71 1/2	40



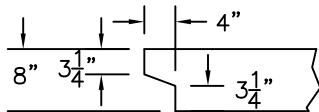
PLAN VIEW



SECTION VIEW



TYPICAL BOLT CONNECTION



TYPICAL JOINT DETAIL

NOTES:

1. CONCRETE: 5,000 PSI MINIMUM AFTER 28 DAYS.
2. DESIGN CONFORMS WITH 310 CMR 15.00, DEP TITLE 5 REGS, FOR SEPTIC TANKS.
3. ALL REINFORCEMENT PER ASTM A-615
4. DESIGNED H-20 LOADING, 2 TO 5 FEET COVER.
5. TEES AND BAFFLES SOLD SEPARATELY.
6. TONGUE AND GROOVE JOINT SEALED WITH BUTYL RESIN AND BOLTED WITH 3/4" DIA BOLTS.

GALLONS	A (LENGTH)	B (LENGTH)	C (BAFFLE)	WEIGHT
13,000	26'-3"	24'-11"	9'-0"	103,950#
14,000	28'-2"	26'-10"	9'-0"	110,386#
15,000	30'-1"	28'-9"	9'-8"	116,822#
16,000	32'-0"	30'-8"	10'-8"	123,258#
17,000	33'-11"	32'-7"	10'-11"	129,694#
18,000	35'-10"	34'-6"	11'-7"	136,130#
19,000	37'-9"	36'-5"	12'-2"	142,566#
20,000	39'-8"	38'-4"	12'-10"	149,002#
21,000	41'-7"	40'-7"	13'-5"	155,438#
22,000	43'-6"	42'-2"	14'-1"	161,874#
23,000	45'-5"	44'-1"	14'-4"	168,310#
24,000	47'-4"	46'-0"	14'-4"	174,746#



New England's Premier Precaster
800-696-7432 (SHEA)
www.sheaconcrete.com

TUNNEL TANK
13,000 GALLON AND UP

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Wilmington, MA 01887

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P.O. Box 807
Amesbury, MA 01913

160 Old Turnpike Road
Nottingham, NH 03290

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tunneltank.dwg

10/31/2003



